

EXERCICE 7-3

11

d) Bilan

* Pesanteur en G: $\vec{P}_T \begin{vmatrix} +mg \sin \alpha \\ -mg \cos \alpha \\ 0 \end{vmatrix} \quad \vec{M}_{R_T}(G) = \vec{0}$

* Pesanteur en C: $\vec{P}_D \begin{vmatrix} +Mg \sin \alpha \\ -Mg \cos \alpha \\ 0 \end{vmatrix} \quad \vec{M}_{P_D}(C) = \vec{0}$

* Action en A: $\vec{R}_A \begin{vmatrix} T_A \\ N_A \\ 0 \end{vmatrix} \quad \vec{M}_A(A) = \vec{0}$

* Action en I: $\vec{R}_I \begin{vmatrix} T_I \\ N_I \\ 0 \end{vmatrix} \quad \vec{M}_I(I) = \vec{0}$

2) Resultante $\vec{P} = \vec{P}_T + \vec{P}_D$ voir schéma

3) On suppose être à la limite du glissement au point I, l'action $\vec{R}_I$ se trouve sur le cône de frottement. Pour que le jouet soumis à $\vec{P}, \vec{R}_I, \vec{R}_A$ soit en équilibre il faut que les trois directions de ces forces soient coplanaires. d'où on déduit $\Delta \vec{R}_A$, et donc φ_a

4) l'équilibre est impossible car $\varphi_a > 45^\circ$ et donc $\mu > 1$.

5) mouvement de (T) = translation. $\Rightarrow \vec{R}_T = \vec{0}$

6) $\mathbb{I}(A, T, b_2) \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{mL^2}{4} & 0 \\ 0 & 0 & \frac{mL^2}{3} \end{bmatrix} \quad \vec{A}_{GT} = \begin{vmatrix} a = L/2 \\ b = 0 \\ c = 0 \end{vmatrix}$

$AA = AGT + m(b^2 + c^2) \Rightarrow AGT = AA$

$BA = BGT + m(a^2 + c^2) \Rightarrow BGT = BA - m \frac{L^2}{4} = \frac{mL^2}{12}$

$CA = CGT + m(a^2 + b^2) \Rightarrow CGT = CA - m \frac{L^2}{4} = \frac{mL^2}{12}$

$DA = DGT + m b c \Rightarrow DGT = DA$

$EA = EGT + m a c \Rightarrow EGT = EA$

$FA = FGT + m a b \Rightarrow FGT = FA$

$\Rightarrow \mathbb{I}(G, T, b_2) \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{mL^2}{12} & 0 \\ 0 & 0 & \frac{mL^2}{12} \end{bmatrix}$

$$7) * \vec{R}_T(V) = m \vec{V}_{GT}$$

$$\vec{O}_{GT} = \vec{OC} + \vec{CGT} = m \vec{m}_0 + R \vec{y}_0 = \frac{L}{2} \vec{m}_2$$

$$\vec{V}_{GT} = \dot{m} \vec{m}_0$$

$$* \vec{\nabla}_T(F) = \mathbb{I}(G_T, T, h_2) \cdot \vec{\Omega}_T = \vec{0}$$

$$\vec{\nabla}_T(C) = \vec{\nabla}_T(G_T) + \vec{R}_T(V) \wedge \vec{G}_T C$$

$$= \vec{0} + m \dot{m} \vec{m}_0 \wedge \frac{L}{2} \vec{m}_2$$

$$= m \frac{L}{2} \dot{m} \sin \theta \vec{z}$$

$$\Rightarrow \begin{cases} \vec{R}_T(V) = m \dot{m} \vec{m}_0 \\ \vec{\nabla}_T(C) = m \frac{L}{2} \dot{m} \sin \theta \vec{z} \end{cases}$$

$$8) * \vec{R}_T(V) = m \vec{V}_{GT} = m \dot{m} \vec{m}_0$$

$$* \vec{O}_T(C) = \frac{d \vec{\nabla}_T(C)}{dt} + m \vec{V}_{GT} \wedge \vec{V}_C$$

$$= m \frac{L}{2} \ddot{m} \sin \theta \vec{z} + \underbrace{m \dot{m} \vec{m}_0 \wedge \dot{m} \vec{m}_0}_{\vec{0}}$$

$$\Rightarrow \begin{cases} \vec{R}_T(V) = m \dot{m} \vec{m}_0 \\ \vec{O}_T(C) = m \frac{L}{2} \ddot{m} \sin \theta \vec{z} \end{cases}$$

$$9) E_{GT} = \frac{1}{2} m \vec{V}_{GT}^2 + \frac{1}{2} \vec{\Omega}_T \cdot \vec{I}_{GT}$$

$$= \frac{1}{2} m \dot{m}^2$$

10) Non calculable pour cause de glissement en A

$$11) \text{ Dû à la Translation + Rotation } = \vec{\Omega}_D = \dot{\theta} \vec{z}$$

$$12) \vec{L}_{DP} = \vec{V}_{IDP} \cdot \vec{V}_{IDP}$$

$$\vec{V}_{IDP} = \vec{V}_C + \vec{\Omega}_D \wedge \vec{CI} = \dot{m} \vec{m}_0 + \dot{\theta} \vec{z} \wedge -R \vec{y}_0 = (\dot{m} + R \dot{\theta}) \vec{m}_0$$

$$\text{CRSG: } \dot{m} + R \dot{\theta} = 0$$

$$13) * \vec{R}_D(V) = M \vec{V}_C = M \dot{m} \vec{m}_0$$

$$* \vec{V}_D(C) = \mathbb{I}(C, D, h_1) \vec{\Omega}_D$$

$$= \begin{bmatrix} \frac{MR^2}{4} & 0 & 0 \\ 0 & \frac{MR^2}{4} & 0 \\ 0 & 0 & \frac{MR^2}{2} \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ \dot{\theta} \end{bmatrix}$$

$$\Rightarrow \begin{cases} \vec{R}_D(V) = M \dot{m} \vec{m}_0 \\ \vec{V}_D(C) = \frac{MR^2}{2} \dot{\theta} \vec{z} \end{cases}$$

$$= \frac{MR^2}{2} \dot{\theta} \vec{z}$$

$$14) * \vec{R}_D(\mathcal{C}) = M \vec{a} \cdot \vec{m}_0$$

$$* \vec{\sigma}_D(\mathcal{C}) = \frac{d}{dt} \vec{\sigma}_D(\mathcal{C}) = \frac{MR^2}{2} \ddot{\theta} \vec{z}$$

$$15) E_C = \frac{1}{2} M \vec{v}_C^2 + \frac{1}{2} \vec{\sigma}_D \cdot \vec{\sigma}_D(\mathcal{C})$$

$$= \frac{1}{2} M \dot{m}^2 + \frac{1}{2} \frac{MR^2}{2} \dot{\theta}^2$$

$$\begin{aligned} h_C &= \vec{\sigma}_C \cdot \vec{y} \\ &= m \vec{a}_0 \cdot \vec{y} + R \vec{y}_0 \cdot \vec{y} \\ &= -m \sin \alpha + c \cdot t. \end{aligned}$$

$$16) E_p = M g h_c + c \cdot t = -M g m \sin \alpha + c \cdot t.$$

non l'hyppothese qu'il y a roulement sans glissement en I!

$$17) (M+m) \vec{CG} = m \vec{CG}_T + M \vec{CC}$$

$$\text{sur } (\vec{m}_2) \quad M+m \vec{CG} \cdot \vec{m}_2 = -m \frac{L}{2} \vec{m}_2 + \vec{0}$$

$$\Rightarrow \vec{CG} = -\frac{mL}{2(M+m)} \vec{m}_2 = -\frac{L}{8} \vec{m}_2$$

$$18) * \vec{R}_J(\mathcal{C}) = \vec{R}_T(\mathcal{C}) + \vec{R}_D(\mathcal{C}) = (M+m) \ddot{m} \vec{m}_0$$

$$* \vec{\sigma}_J(\mathcal{C}) = \vec{\sigma}_T(\mathcal{C}) + \vec{\sigma}_D(\mathcal{C}) = m \frac{L}{2} \ddot{m} \sin \beta \vec{y}_0 + \frac{MR^2}{2} \ddot{\theta} \vec{z}$$

$$= \left(m \frac{L}{2} \ddot{m} \sin \beta + \frac{MR^2}{2} \ddot{\theta} \right) \vec{z}$$

$$19) * E_{CT} = E_{CT} + E_{CD} = \frac{1}{2} (M+m) \dot{m}^2 + \frac{1}{4} MR^2 \dot{\theta}^2$$

$$20) * E_{pj} = E_{pT} + E_D \quad \text{non calculable car y frottement en A.}$$

$$21) - \text{NON} \Rightarrow \text{glissement au point A.}$$

$$22) * \vec{\eta}_{p_T(\mathcal{C})} = \vec{\eta}_{p_T(\mathcal{G}_T)} + \vec{p}_{TA} \vec{GTC}$$

$$\vec{GTC} = \frac{L}{2} \vec{m}_2 = \frac{L}{2} (\cos \beta \vec{m}_0 + \sin \beta \vec{y}_0)$$

$$= \begin{vmatrix} 0 \\ 0 \\ 0 \end{vmatrix} + \begin{vmatrix} +mg \sin \alpha \\ -mg \cos \alpha \\ 0 \end{vmatrix} \begin{vmatrix} \frac{L}{2} \cos \beta \\ \frac{L}{2} \sin \beta \\ 0 \end{vmatrix}$$

$$= +mg \frac{L}{2} (\sin \alpha \sin \beta + \cos \alpha \cos \beta) \vec{z} = mg \frac{L}{2} \cos(\alpha - \beta) \vec{z}$$

$$* \vec{\eta}_{A(\mathcal{C})} = \vec{\eta}_A(\mathcal{A}) + \vec{RA} \vec{AAC} \quad \vec{AC} = L \vec{m}_2$$

$$= \begin{vmatrix} 0 \\ 0 \\ 0 \end{vmatrix} + \begin{vmatrix} T_A \\ N_A \\ 0 \end{vmatrix} \begin{vmatrix} L \cos \beta \\ L \sin \beta \\ 0 \end{vmatrix}$$

$$= L (T_A \sin \beta - N_A \cos \beta) \vec{z}$$

$$* \vec{M}_I(t) = \vec{M}_I(I) + \vec{R}_I \wedge \vec{IC} \quad \vec{IC} = R \vec{y}_0$$

$$= \vec{0} + (\vec{T}_I \vec{a}_0 + N \vec{e}_3 \vec{y}_0) \wedge R \vec{y}_0 = \vec{T}_I \cdot R \vec{z}$$

$$\Rightarrow \vec{R}_{Fext} = \begin{pmatrix} (M+m) g \sin \alpha + T_A + T_I \\ -(M+m) g \cos \alpha + N_A + N_I \\ 0 \end{pmatrix}$$

$$\vec{M}_{Fext}(t) = \left[+ m g \frac{L}{2} \cos(\alpha - \beta) + L(T_A \sin \beta - N_A \cos \beta) + T_I R \right] \vec{z}$$

23) $\vec{R}_{Fext} = \vec{R}_I(t)$

$$\vec{M}_{Fext}(t) = \vec{S}_I(t)$$

$$\Rightarrow \begin{cases} + (M+m) g \sin \alpha + T_A + T_I = (M+m) \ddot{u} \\ - (M+m) g \cos \alpha + N_A + N_I = 0 \\ - m g \frac{L}{2} \cos(\alpha - \beta) + L(T_A \sin \beta - N_A \cos \beta) + T_I R = \frac{ML}{2} \ddot{u} \sin \beta + \frac{MR^2}{2} \ddot{\theta} \end{cases}$$